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# FDMF4061 – High Performance 60V Smart Power Stage Module

#### Features

- Compact size 6.0 mm x 7.5 mm PQFN
- High current handling: 25A
- Next Generation 60V Power MOSFETs:
- Typ.  $R_{DS(on)}$ =2.4(HS) / 2.4(LS) m $\Omega$  at V<sub>GS</sub>=10V, I<sub>D</sub>=25A
- Wide driver power supply voltage range: 10V to 20V
- Internal pull-down resistors for PWM inputs (HI,LI)
- Short PWM propagation delays
- Under-voltage lockout (UVLO)
- Fully optimized system efficiency
- High performance low profile package
- Integrated 60V Half-Bridge gate driver
- Fairchild 60V PowerTrench® MOSFETs for clean switching waveforms and reduced ringing
- Low Inductance and low resistance packaging for minimal operating power losses
- Fairchild green packaging and RoHS compliant
- Reduced EMI due to low side flip-chip MOSFET

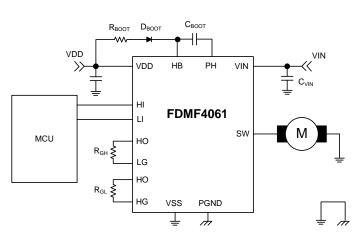
#### **General Description**

The FDMF4061 is a compact 60V Smart Power Stage (SPS) module that is a fully optimized for use in high current switching applications. The FDMF4061 module integrates a driver IC plus two N-channel Power MOSFETs into a thermally enhanced, 6.0 mm x 7.5 mm PQFN package. The PQFN packaging provides very low package inductance and resistance improving the current handling capability and performance of the part. With an integrated approach, the complete switching power stage is optimized with regards to driver and MOSFET dynamic performance, system parasitic inductance, and Power MOSFET RDS(ON). The FDMF4061 uses Fairchild's high performance PowerTrench<sup>™</sup> MOSFET technology, which reduces high voltage and current stresses in switching applications. The driver IC features a low delay times and matched PWM input propagation delays, which further enhance the performance of the part.

#### Applications

- Motor Drives (Power tools & Drowns etc.)
- Telecom Half / Full Bridge DC-DC converters
- Buck-Boost Converters
- High-current DC-DC Point of Load (POL) converters.

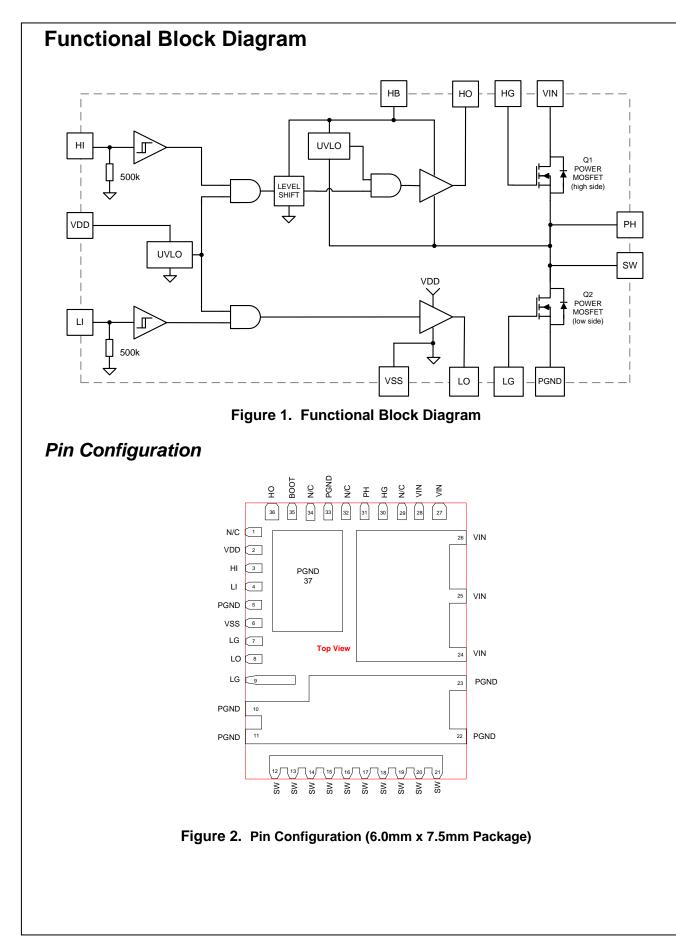
#### **Application Diagram**



#### **Ordering Information**

| Part Number | Current Rating<br>[A] | Input Voltage<br>[V] | Frequency Max<br>[kHz] | Device Marking |
|-------------|-----------------------|----------------------|------------------------|----------------|
| FDMF4061    | 25                    | 60                   | 200                    | FDMF4061       |

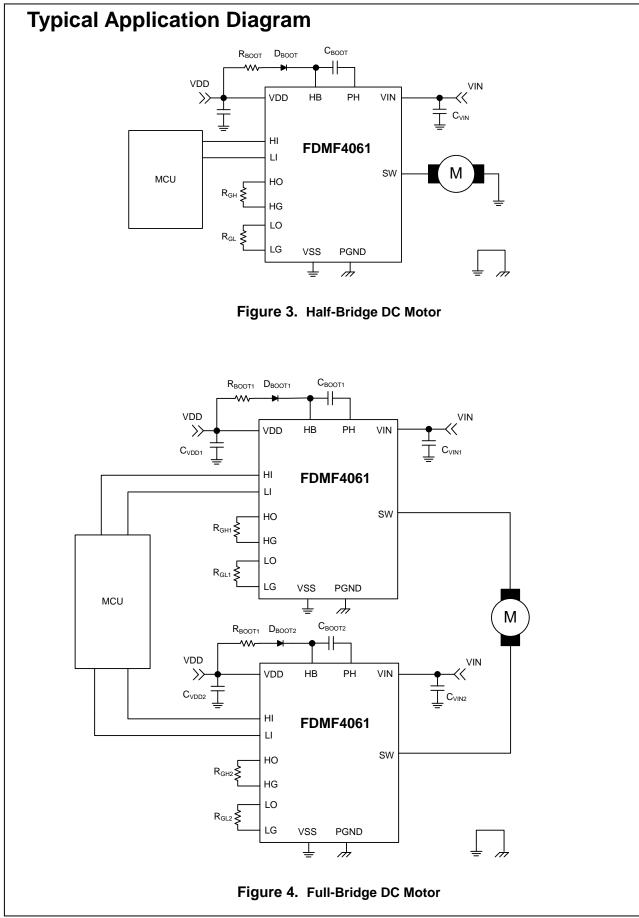


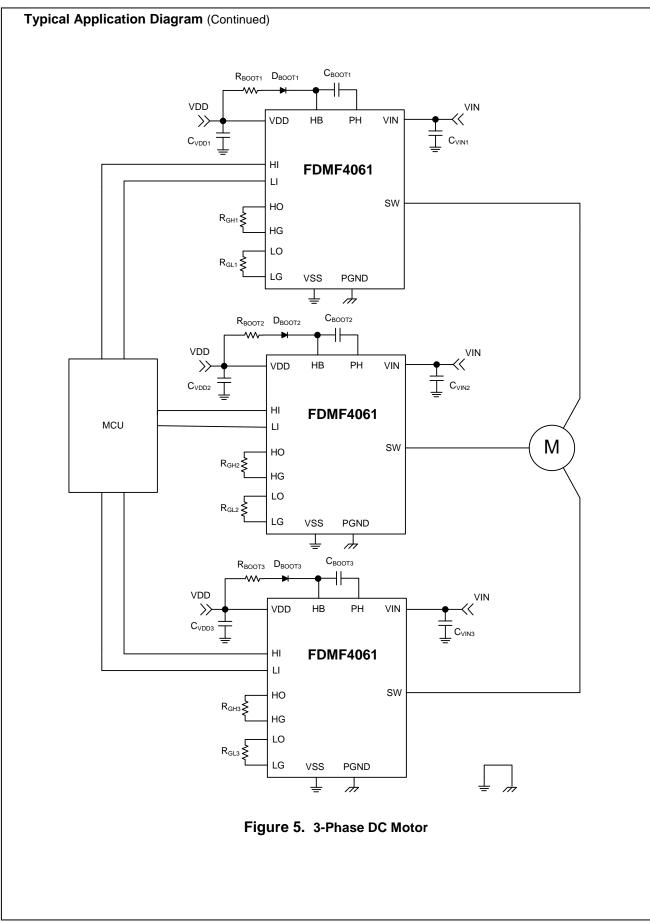


# Pin Definitions

| Pin                         | Name | Function   |
|-----------------------------|------|--|
| 1, 29, 32, 34               | N/C  | No connect   |
| 2                           | VDD  | Power supply input for low-side gate drive and bootstrap diode. Bypass this pin to VSS with a low impedance capacitor. |
| 3                           | н    | High-side PWM input.   |
| 4                           | LI   | Low-side PWM input.  |
| 5, 10,11, 22,<br>23, 33, 37 | PGND | Power return for the power stage. Package header, pin 37 and PGND are internally fused (shorted).                      |
| 6                           | VSS  | Analog ground for driver IC analog circuits.   |
| 7,9                         | LG   | Low-side MOSFET gate.  |
| 8                           | LO   | Low-side gate drive output.  |
| 12-21                       | SW   | Switching node junction between high-side and Low-side MOSFETs.  |
| 24-28                       | VIN  | Power input for the power stage. Bypass this pin to PGND with low impedance capacitor.                                 |
| 30                          | HG   | High-side MOSFET gate.   |
| 31                          | PH   | High-side source connection (SW node) for the bootstrap capacitor.   |
| 35                          | HB   | Bootstrap supply for high-side driver. Bypass this pin to PH with low impedance capacitor.                             |
| 36                          | НО   | High-side gate drive output.   |

## Table 1. Pin Definitions





# FDM4061 - High Performance 60V Smart Power Stage Module

#### Typical Application Diagram (Continued)

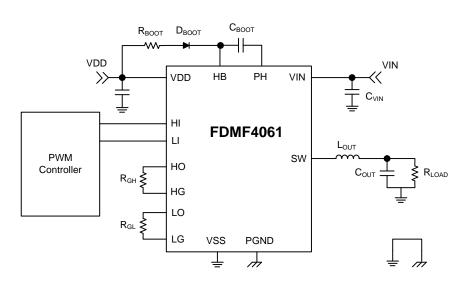


Figure 6. Buck Converter

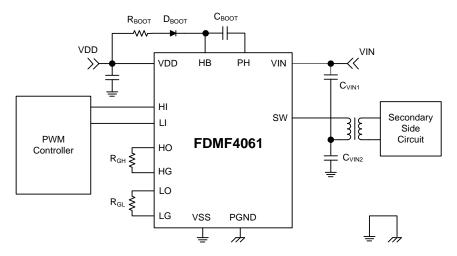
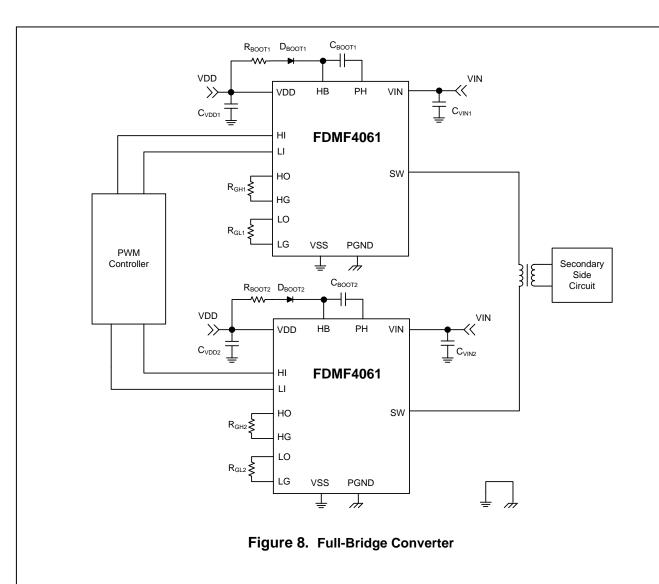


Figure 7. Half-Bridge Converter

Typical Application Diagram (Continued)



# **Absolute Maximum Ratings**

The "Absolute Maximum Ratings" are those values beyond which the safety of the device cannot be guaranteed. The device should not be operated at these limits. The parametric values defined in the Electrical Characteristics tables are not guaranteed at the absolute maximum ratings. The "Recommended Operating Conditions" table defines the conditions for actual device operation. Thermal resistance rating is measured under board mounted and still air conditions.

| Symbol                        | Pa                              | arameter                     | Min.                   | Max.                     | Unit |
|-------------------------------|---------------------------------|------------------------------|------------------------|--------------------------|------|
| V <sub>IN</sub>               | Power Stage Supply Voltage      | Referenced to VSS            | -0.3                   | 60                       | V    |
| $V_{PH}$                      | PH Voltage                      | Referenced to VSS            | V <sub>HB</sub> -25    | V <sub>HB</sub> +0.3     | V    |
| V <sub>DD</sub>               | Driver Supply Voltage           | Referenced to VSS            | -0.3                   | 25                       | V    |
| $V_{\text{HB}}$               | Bootstrap to VSS                | Referenced to VSS,           | -0.3                   | 85                       | V    |
| $V_{\text{LI},}V_{\text{HI}}$ | Gate drive Input signals        | Referenced to VSS            | -0.3                   | V <sub>DD</sub> + 0.3V   | V    |
| V <sub>HO</sub>               | High Side driver output         | Referenced to PHASE          | V <sub>PH</sub> - 0.3V | V <sub>BOOT</sub> + 0.3V | V    |
| V <sub>LO</sub>               | Low Side driver output          | Referenced to VSS            | - 0.3                  | V <sub>DD</sub> + 0.3V   | V    |
| $V_{HG}$                      | High Side MOSFET gate           | Referenced to PHASE          | -26                    | 28                       | V    |
| $V_{LG}$                      | Low Side MOSFET gate            | Referenced to VSS            | -26                    | 28                       | V    |
| 0                             | Junction to Ambient Thermal Res | sistance – Q1 <sup>(1)</sup> | -                      | 17                       | °C/W |
| $\Theta_{JA}$                 | Junction to Ambient Thermal Res | sistance – Q2 <sup>(1)</sup> | -                      | 15                       | °C/W |
| TJ                            | Junction Temperature            |                              | -                      | 150                      | °C   |
| T <sub>STG</sub>              | Storage Temperature             |                              | -40                    | 150                      | °C   |

#### Table 2. Module Absolute Maximum ratings

(1) Mounted on a 4-layer FR4 PCB with a dissipating copper surface on the top side of 49 cm2, 2oz.

# **Recommended Operating Conditions**

| Symbol               | Parameters                 | Test Condition                  | Min                  | Max                  | Unit |
|----------------------|----------------------------|---------------------------------|----------------------|----------------------|------|
| V <sub>IN</sub>      | Power Stage Supply Voltage |                                 | 3                    | 50                   | V    |
| V <sub>DD</sub>      | Driver Supply Voltage      |                                 | 10                   | 20                   | V    |
|                      | SW or PHASE                | DC                              | -0.3                 | 60                   | V    |
| $V_{SW}, V_{PH}$     |                            | Repetitive Pulse (< 20ns, 10uJ) | 6-V <sub>DD</sub>    | 60                   | V    |
| V <sub>HB</sub>      | Voltage on HB              | Reference to PH                 | V <sub>PH</sub> + 10 | V <sub>PH</sub> + 20 | V    |
| dV <sub>sw</sub> /dt | Voltage Slew Rate on SW    |                                 | -                    | 50                   | V/ns |
| TJ                   | Operating Temperature      |                                 | -40                  | 125                  | °C   |

 Table 3. Module Recommended Operating Conditions

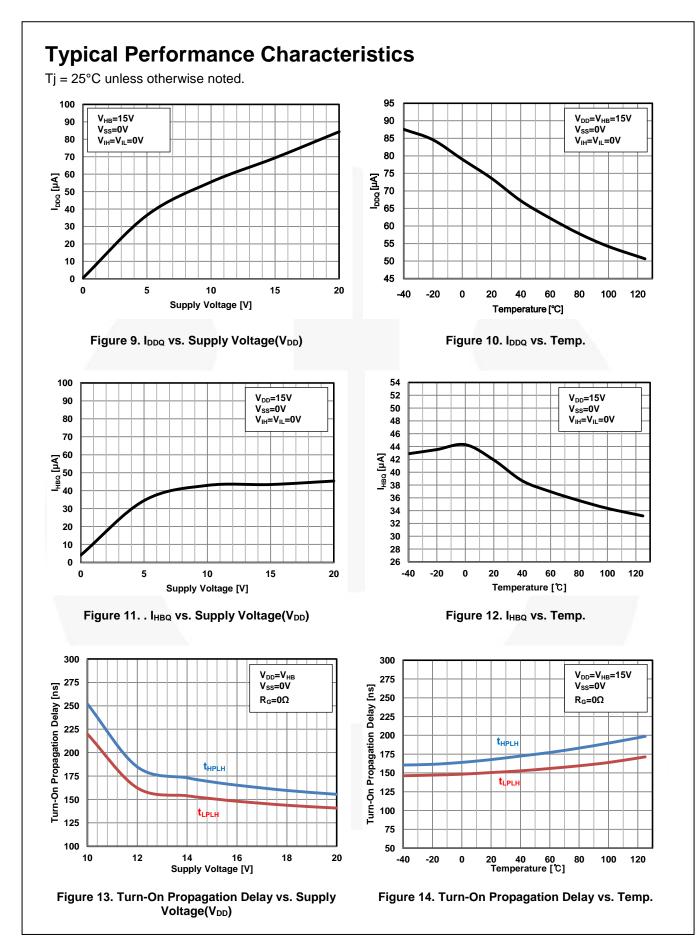
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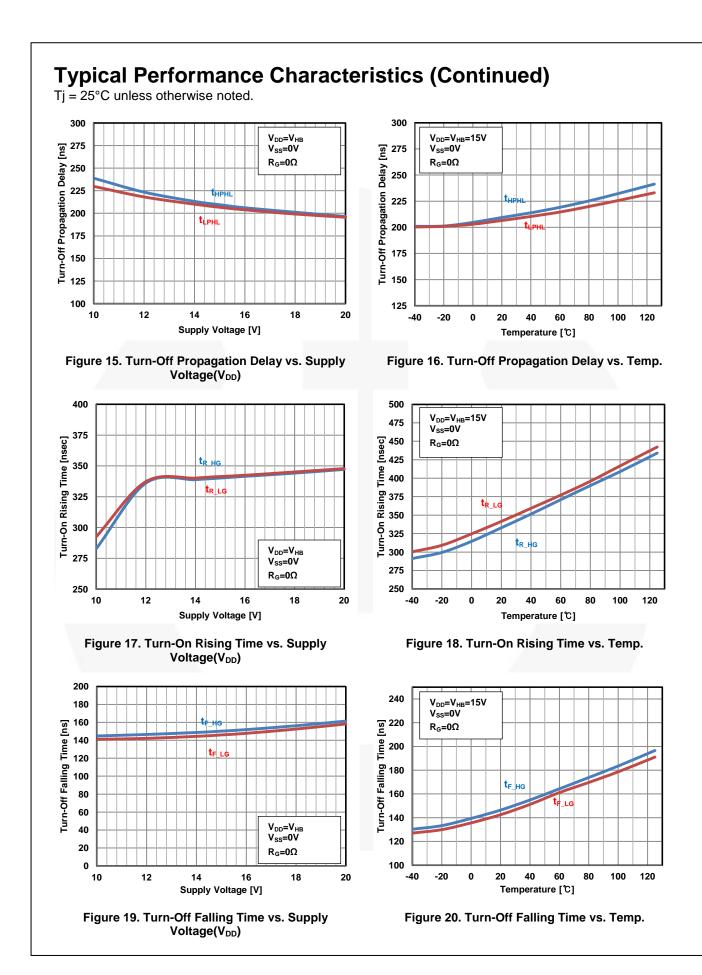
| Symbol  | Parameter  | Condition  | Min. | Тур. | Max. | Unit |
|---|--|--|------|------|------|------|
| Supply Curi   | rents  |  |      |      |      | 1    |
| I <sub>INQ</sub>  | Power Stage Quiescent Current                        | LI = HI = 0V   | -    | -    | 1    | uA   |
| IDDQ  | Driver Quiescent Current                             | LI = HI = 0V   | -    | 67   | 180  | uA   |
|   |  | F <sub>SW</sub> = 20kHz  | -    | 0.3  | 0.6  | mA   |
| I <sub>DDO</sub>  | VDD operating current                                | F <sub>SW</sub> = 200kHz   | -    | 2.1  | 4.2  | mA   |
| I <sub>HBQ</sub>  | BOOT Quiescent current                               | LI = HI = 0V   | -    | 38   | 120  | uA   |
| 1   | BOOT Operating current                               | F <sub>SW</sub> = 20kHz  | -    | 0.3  | 0.6  | mA   |
| I <sub>HBO</sub>  | BOOT Operating current                               | F <sub>SW</sub> = 200kHz   | -    | 2.4  | 4.8  | mA   |
| Under-Volta   | ge Protection  |  |      |      |      |      |
| $V_{\text{DDR},} V_{\text{HBR}}$  | UVLO rising threshold                                | $V_{\text{DD}} \text{ or } V_{\text{HB}} \text{-} V_{\text{PH}}$ rising threshold    | 8.2  | 9.5  | 10.0 | V    |
| $V_{\text{DDF},}V_{\text{HBF}}$   | UVLO falling threshold                               | $V_{\text{DD}}$ or $V_{\text{HB}}\text{-}V_{\text{PH}}$ falling Threshold            | 7.6  | 8.9  | 9.6  | V    |
| V <sub>DDH</sub>  | UVLO Hysteresis                                      | V <sub>DD</sub> Hysterisis   |      | 0.6  | -    | V    |
| $t_{D_{POR}}$   | POR delay to Enable IC                               | UVLO rising to internal PWM enable   | -    | -    | 10   | us   |
| Control Inp   | uts (TTL: LI, HI)                                    |  |      |      |      |      |
| VIL   | Low Level Input Voltage                              |  | 1.2  | -    | -    | V    |
| V <sub>IH</sub>   | High Level Input Voltage                             | $V_{DD} = 10V$ to 20V  | -    | -    | 2.9  | V    |
| V <sub>HYS</sub>  | Input Voltage Hysteresis                             |  | -    | 1.0  | -    | V    |
| R <sub>IN</sub>   | Input Pull-Down Resistance                           |  | -    | 468  | -    | kΩ   |
| PWM input   | (HI,LI)  |  |      |      |      |      |
| t <sub>LPLH</sub>   | LI to LO Propagation Delays                          | LI Low $\rightarrow$ HIGH to LO Low $\rightarrow$ HIGH,<br>V <sub>IH</sub> to 10% LG | 100  | 153  | 300  | ns   |
| t <sub>LPHL</sub>   |  | LI <i>High→Low</i> to LO <i>High→Low</i> , V <sub>IL</sub> to 90% LG                 | 100  | 208  | 300  | ns   |
| t <sub>HPLH</sub>   |  | HI <i>Low→HIGH</i> to HO<br><i>Low→HIGH</i> ,V <sub>IH</sub> to 10% HG-PH            | 100  | 170  | 300  | ns   |
| t <sub>HPHL</sub>   | HI to HO Propagation Delays                          | HI <i>High→Low</i> to HO <i>High→Low</i> ,<br>V <sub>IL</sub> to 90% HG-PH           | 100  | 205  | 300  | ns   |
| MT  | Delay matching, HS and LS turn-on/off                |  | -    | -    | 50   | ns   |
|   | Minimum Input Pulse Width that<br>Changes the Output | LI/HI Rising to Vth of Q1,Q2 $R_{\rm G}{=}0\Omega$                                   |      | 75   |      | ns   |
| t <sub>PW</sub>   |  | LI/HI Falling to Vth of Q1,Q2 $R_G=0\Omega$  |      | 130  |      | ns   |
| High-Side D   | vriver (HDRV) (VDD = VHB = 15V)                      |  |      |      |      | 1    |
| I <sub>SOURCE_HO</sub>  | Output Sourcing Peak current                         | V <sub>HO</sub> =0V  | 250  | 350  | -    | mA   |
| I <sub>SINK_HO</sub>  | Output Sinking Peak current                          | V <sub>HO</sub> =15V   | 500  | 650  | -    | mA   |
| t <sub>R_HG</sub>   | Rise Time  | GH=10% to 90%, R <sub>GH</sub> =0Ω   | -    | 356  | 711  | ns   |
| t <sub>F HG</sub>   | Fall Time  | GH=90% to 10%, $R_{GH}=0\Omega$  | -    | 151  | 302  | ns   |
|   | river (LDRV) (VDD = VHB = 15V)                       | 1  |      | 1    | L    | 1    |
| ISOURCE LO  | Output Sourcing Peak current                         | V <sub>LO</sub> =0V  | 250  | 350  | -    | mA   |
| I <sub>SINK LO</sub>  | Output Sinking Peak current                          | V <sub>L0</sub> =15V   | 500  | 650  | _    | mA   |
|   | Rise Time  | GL=10% to 90%, R <sub>GL</sub> =0Ω   | -    | 346  | 692  | ns   |
| <r_lg< td=""><td></td><td>CL-10/0 10 00/0, 11GL-012</td><td></td><td>5-0</td><td>002</td><td>113</td></r_lg<> |  | CL-10/0 10 00/0, 11GL-012  |      | 5-0  | 002  | 113  |

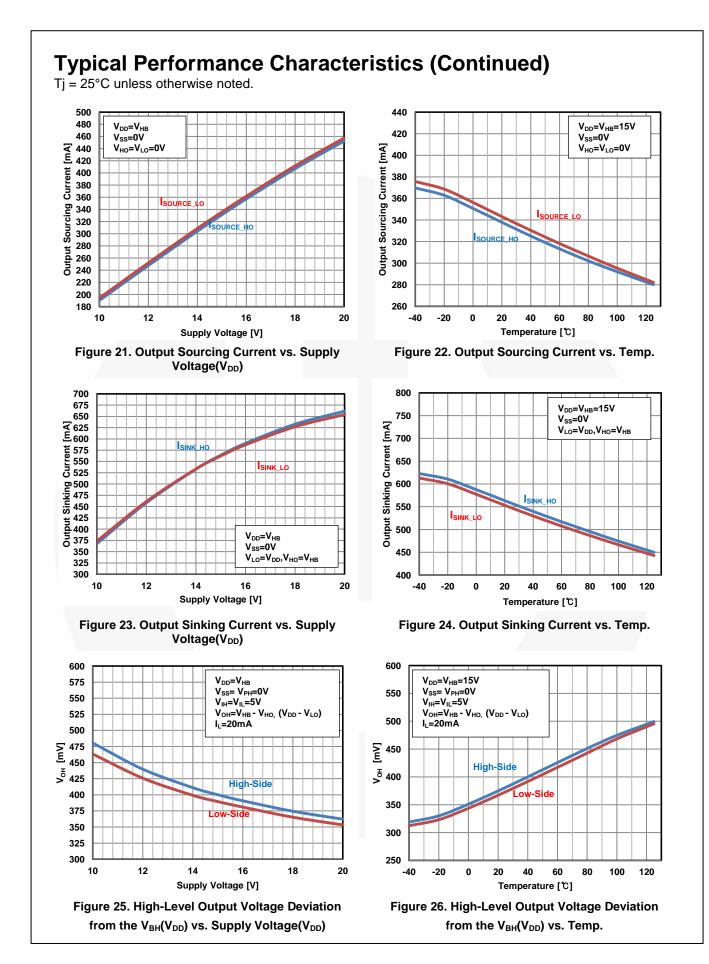
# **Electrical Specifications:**

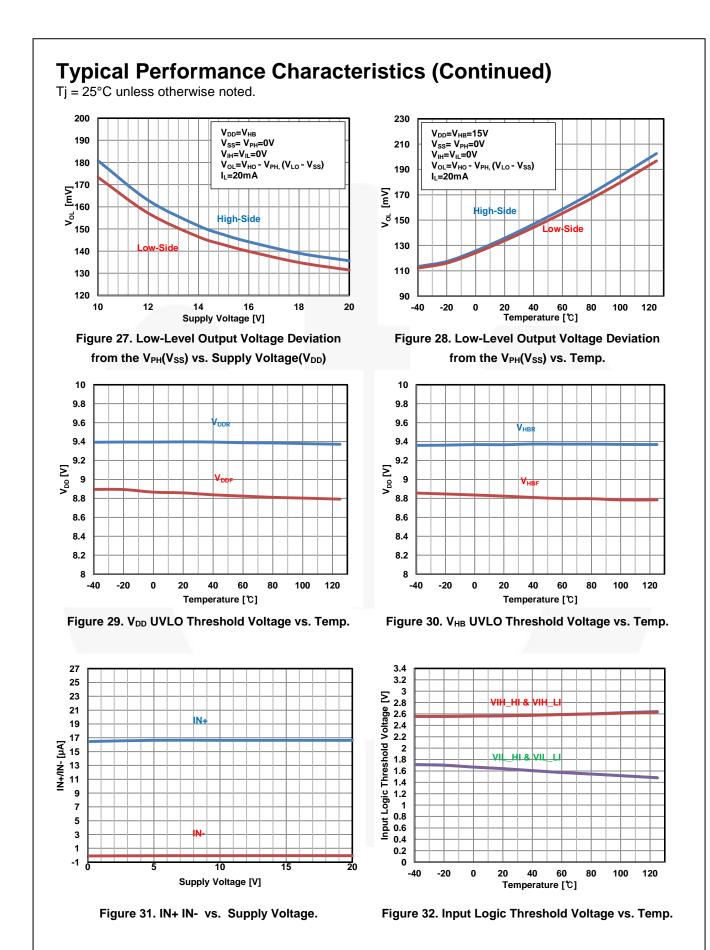
| -                   | °C unless otherwise noted.      |  |      | r    | 1    |       |
|---------------------|---------------------------------|--|------|------|------|-------|
| Symbol              | Parameter                       | Condition  | Min. | Тур. | Max. | Unit  |
| High Side           | e MOSFET, Q1                    |  |      |      |      |       |
| $BV_{DSS}$          | Drain-Source Breakdown Voltage  | I <sub>DS</sub> =250uA, V <sub>GS</sub> =0V                            | 60   | -    | -    | V     |
| I <sub>DSS</sub>    | Zero Gate Voltage Drain Current | V <sub>DS</sub> =48V, V <sub>GS</sub> =0V                              | -    | -    | 1    | uA    |
| I <sub>GSS</sub>    | Gate-Source Leakage Current     | V <sub>DS</sub> =0V, V <sub>GS</sub> =+/-20V                           | -    | -    | 100  | nA    |
| V <sub>GS(th)</sub> | Gate-Source Threshold Voltage   | V <sub>DS</sub> =V <sub>GS</sub> , I <sub>DS</sub> =250uA              | 2.5  | 3.7  | 4.5  | V     |
| R <sub>DS(ON)</sub> | Drain –Source On-Resistance     | V <sub>GS</sub> =10V, I <sub>DS</sub> =25A                             | -    | 2.4  | 3.2  | mΩ    |
| Q <sub>G</sub>      | Total Gate Charge               |  | -    | 56   | 78   | nC    |
| Q <sub>GS</sub>     | Gate-Source Charge              |  | -    | 23   | -    | nC    |
| Q <sub>GD</sub>     | Gate-Drain "Miller" Charge      | $V_{GS}=0V$ to 10V, $V_{DD}=30V$ , $I_{DS}=25A$                        | -    | 8    | -    | nC    |
| Q <sub>OSS</sub>    | Total Output Charge             |  | -    | 65   | -    | nC    |
| R <sub>G</sub>      | Series Gate Resistance          |  | -    | 1.0  | -    | Ω     |
| Drain-So            | burce Diode Characteristics     |  | •    | •    | •    |       |
|                     |                                 | $V_{HG}$ - $V_{PH}$ =0V, $I_{SD}$ = 2A                                 | -    | 0.7  | 1.2  |       |
| $V_{SD}$            | Source to Drain Forward Voltage | $V_{HG}-V_{PH}=0V, I_{SD}=25A$   | -    | 0.8  | 1.3  | V     |
| t <sub>RR</sub>     | Reverse Recovery Time           |  | -    | 58   | 117  | ns    |
| Q <sub>RR</sub>     | Reverse Recovery Charge         | I <sub>F</sub> = 25A, di <sub>F</sub> /dt = 100A/us                    | -    | 51   | 103  | nC    |
| t <sub>RR</sub>     | Reverse Recovery Time           |  | -    | 44   | 88   | ns    |
| $Q_{\text{RR}}$     | Reverse Recovery Charge         | I <sub>F</sub> = 25A, di <sub>F</sub> /dt = 300A/us                    | -    | 79   | 158  | nC    |
| Low Side            | MOSFET, Q2                      |  |      | •    |      |       |
| BV <sub>DSS</sub>   | Drain-Source Breakdown Voltage  | I <sub>DS</sub> =250uA, V <sub>GS</sub> =0V                            | 60   | -    | -    | V     |
| I <sub>DSS</sub>    | Zero Gate Voltage Drain Current | V <sub>DS</sub> =48V, V <sub>GS</sub> =0V                              | -    | -    | 1    | uA    |
| I <sub>GSS</sub>    | Gate-Source Leakage Current     | V <sub>DS</sub> =0V, V <sub>GS</sub> =+/-20V                           | -    | -    | 100  | nA    |
| V <sub>GS(th)</sub> | Gate-Source Threshold Voltage   | V <sub>DS</sub> =V <sub>GS</sub> , I <sub>DS</sub> =250uA              | 2.5  | 3.5  | 4.5  | V     |
| R <sub>DS(ON)</sub> | Drain –Source On-Resistance     | V <sub>GS</sub> =10V, I <sub>DS</sub> =25A                             | -    | 2.4  | 3.2  | mΩ    |
| $Q_{G}$             | Total Gate Charge               |  | -    | 59   | 82   | nC    |
| $Q_{GS}$            | Gate-Source Charge              | V <sub>GS</sub> =0V to 10V, V <sub>DD</sub> =30V, I <sub>DS</sub> =25A | -    | 25   | -    | nC    |
| $Q_{GD}$            | Gate-Drain "Miller" Charge      |  | -    | 11   | -    | nC    |
| Q <sub>OSS</sub>    | Total Output Charge             |  | -    | 63   | -    | nC    |
| R <sub>G</sub>      | Series Gate Resistance          |  | -    | 1.0  | -    | Ω     |
| Drain-So            | ource Diode Characteristics     |  | 1    | 1    | 1    | 1     |
| V <sub>SD</sub>     | Source to Drain Forward Voltage | $V_{HG}$ - $V_{PH}$ =0V, $I_{SD}$ = 2A                                 | -    | 0.7  | 1.2  | v     |
| • 30                |                                 | $V_{HG}$ - $V_{PH}$ =0V, $I_{SD}$ = 25A                                | -    | 0.8  | 1.3  | ,<br> |
| t <sub>RR</sub>     | Reverse Recovery Time           | I <sub>F</sub> = 25A, di <sub>F</sub> /dt = 100A/us                    | -    | 57   | 114  | ns    |
| Q <sub>RR</sub>     | Reverse Recovery Charge         |  | -    | 52   | 105  | nC    |
| t <sub>RR</sub>     | Reverse Recovery Time           | I <sub>F</sub> = 25A, di <sub>F</sub> /dt = 300A/us                    | -    | 43   | 86   | ns    |
| Q <sub>RR</sub>     | Reverse Recovery Charge         | $r_{\rm F} = 2000,  {\rm dir}/{\rm dt} = 00000000$                     | -    | 81   | 161  | nC    |

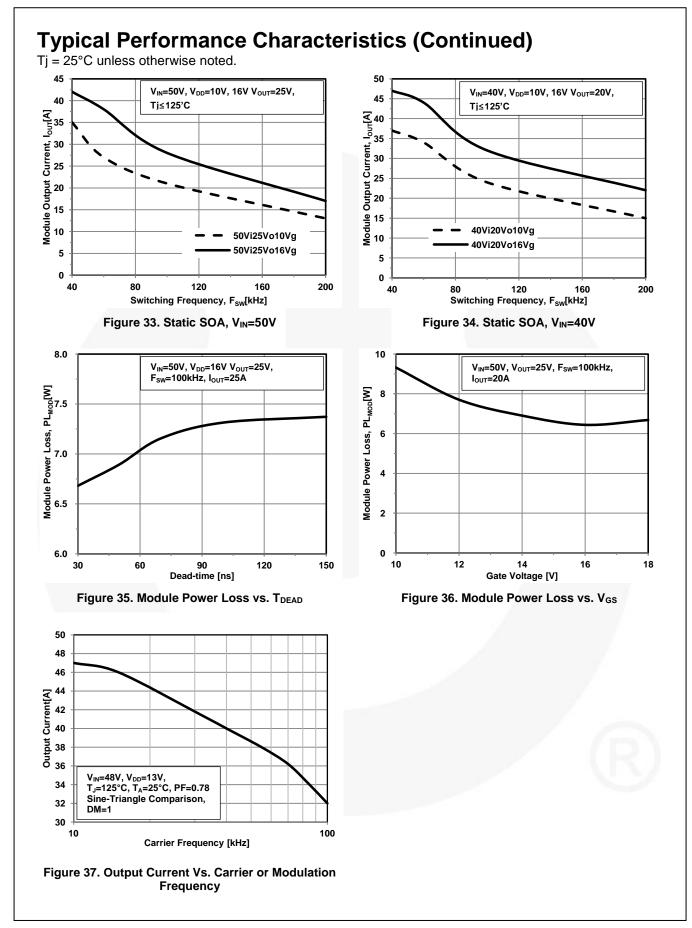
## Table 5. FDMF4061 MOSFET Electrical Specifications

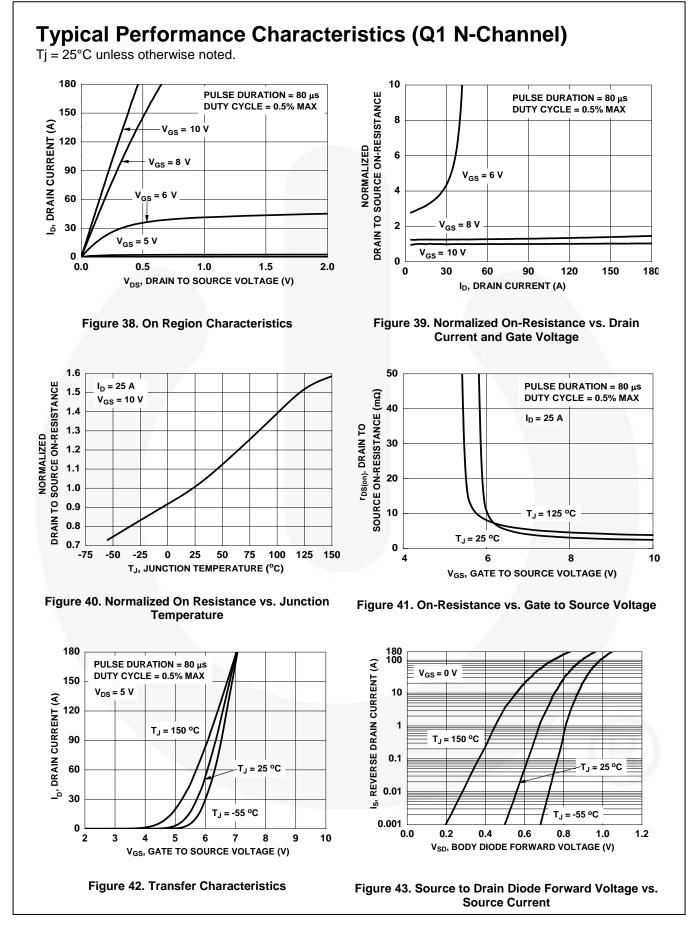








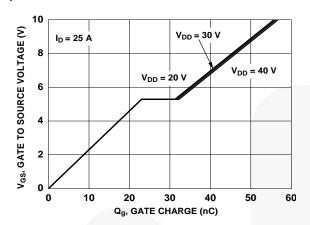




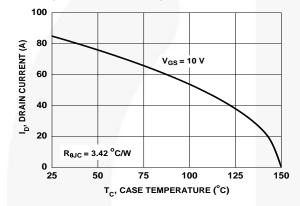


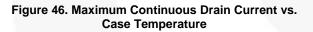
# **Typical Performance Characteristics (Q1 N-Channel)**

 $T_j = 25^{\circ}C$  unless otherwise noted.









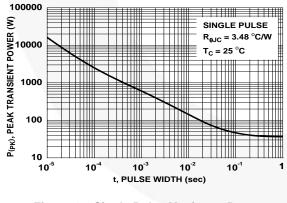


Figure 48. Single Pulse Maximum Power Dissipation

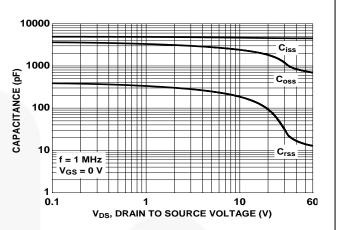
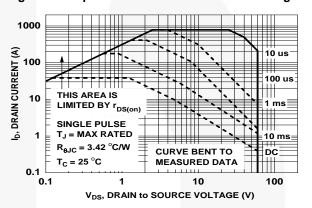
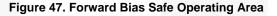
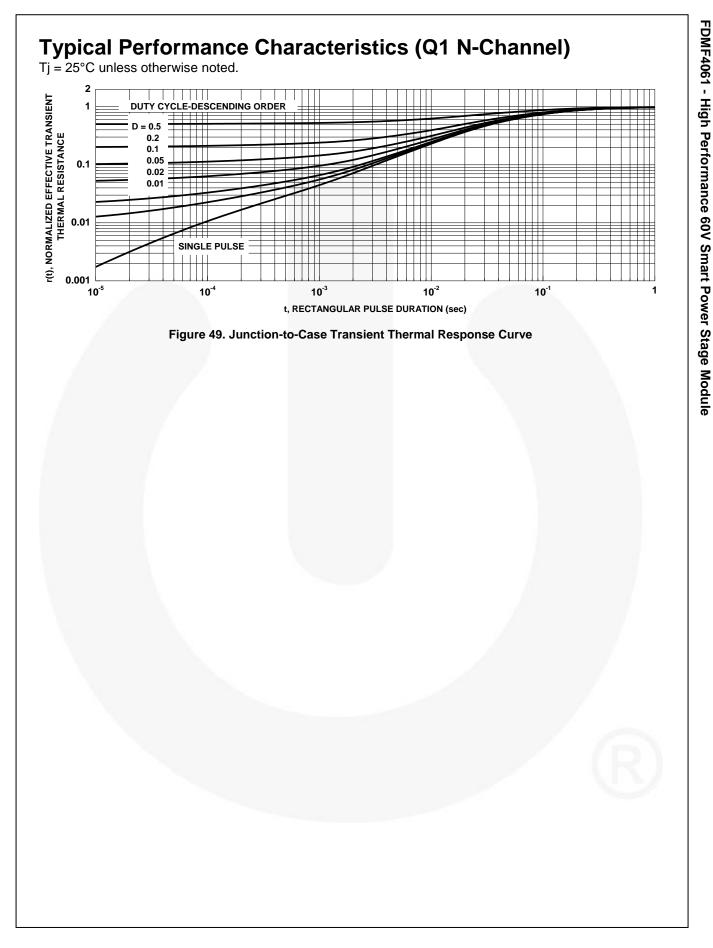
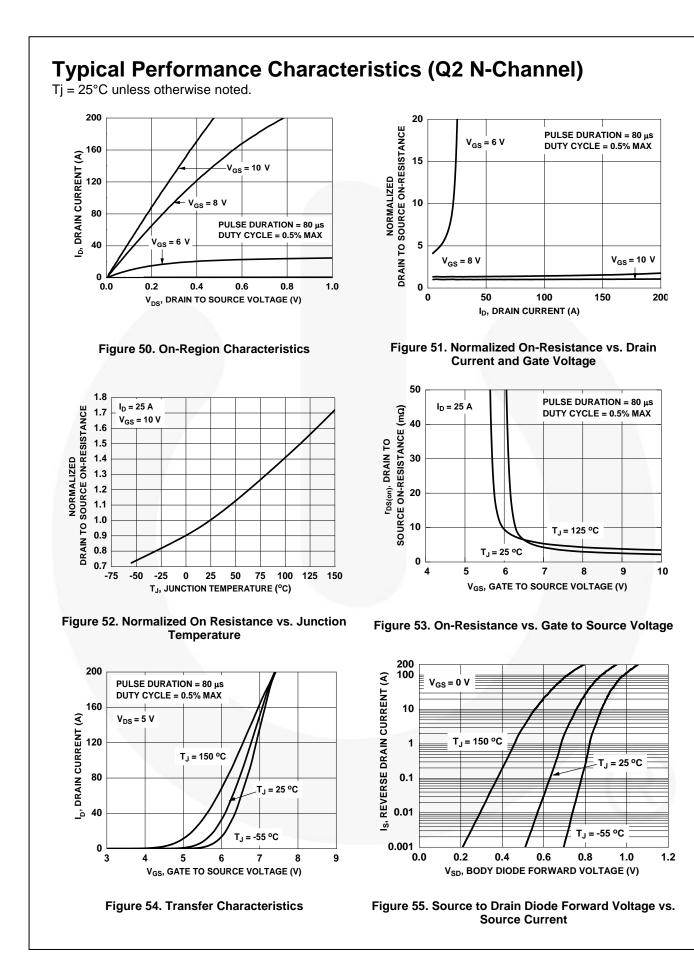


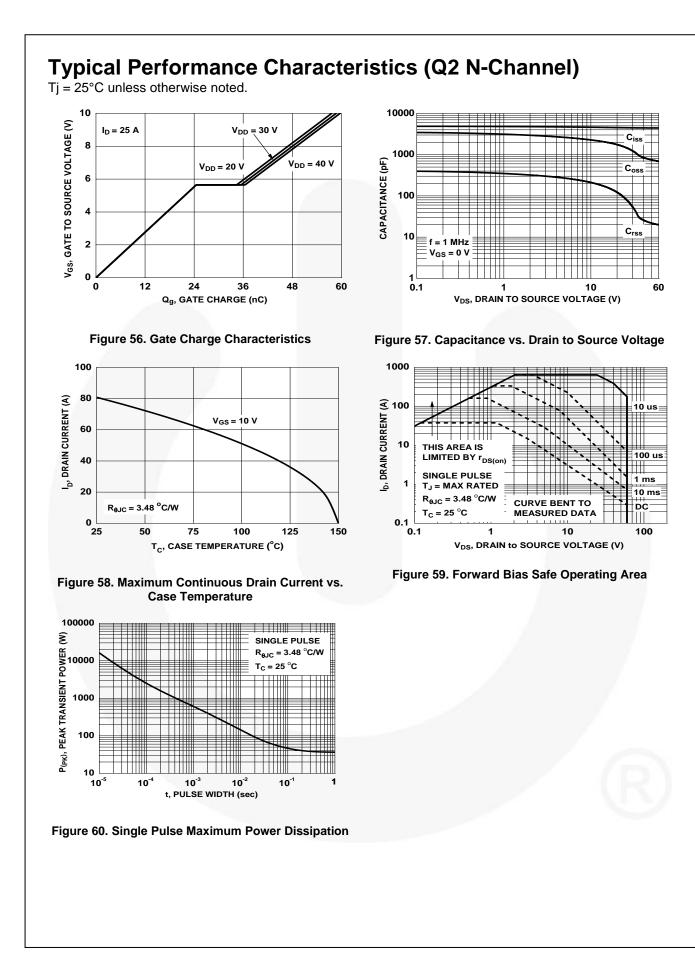
Figure 45. Capacitance vs. Drain to Source Voltage

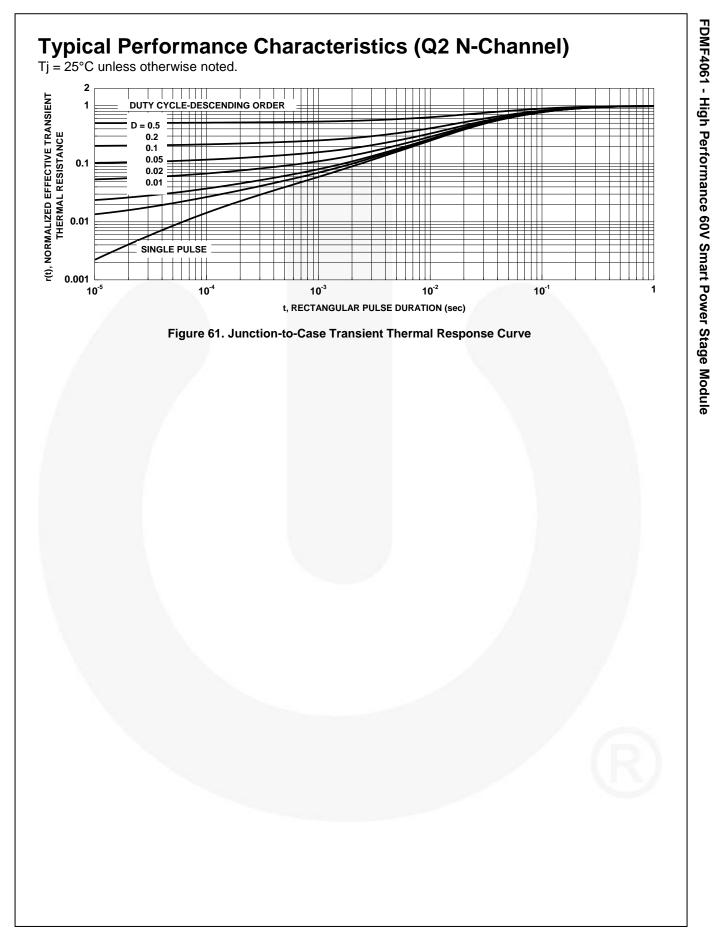












# **Functional Description**

The FDMF4061 is a non-inverting 60V halfbridge Smart Power Stage (SPS) module. The module packages a driver IC die along with pair of equally sized (matched  $R_{DSON}$ ) 60V PowerTrench<sup>TM</sup> N-Channel MOSFETs (Standard gate thresholds refer to **Table 5**).

The FDMF4061 module provides separate power input pins; the power stage input (VIN) and the gate driver input (VDD). The power stage input (VIN) accepts a wide operating from 3V to 50V, while the gate driver input (VDD) requires 10V to 20V. The module accepts TTL compatible inputs (HI/LI) along with anti-cross conduction circuitry to protect against over-lapping PWM (HI/LI) pulses. The module (driver IC) also implements UVLO circuitry in both the VDD-VSS and BOOT-PH power domains.

## Power-Up and UVLO Operation

UVLO circuits are implemented in both the VDD-VSS and HB-PH power domains. During power-up, the VDD-VSS UVLO circuit forces HO and LO low until the VDD supply voltage exceeds the UVLO rising threshold (9.2V typ.). The module (driver IC) will begin responding to PWM pulses once VDD exceeds the UVLO threshold. The UVLO circuit does contain hysteresis (~0.6V) to prevent noise from interfering with normal operation. An additional UVLO circuit is implemented on the HB-PH pins which will hold HO low until HB-PH > The HB-PH UVLO (9.2V typ.). also incorporates hysteresis (~0.6V).

| VDD<br>UVLO | BOOT<br>UVLO | Driver State               |
|-------------|--------------|----------------------------|
| 0           | Х            | Disabled (GH, GL=0)        |
| 1           | 0            | GL follows PWM , GH=0)     |
| 1           | 1            | Enabled (GH/GL follow PWM) |

#### Table 6. UVLO Truth Table

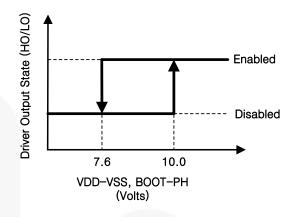
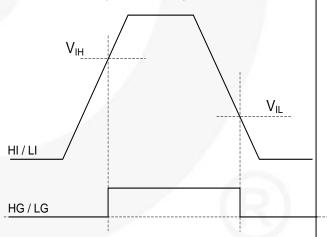


Figure 62. Min/Max UVLO thresholds

## **PWM Input Stage**

The FDMF4061 incorporates a PWM input gate drive design, where the low side drive output (LO) and high side drive output (HO) are controlled through independent PWM inputs (LI and HI, respectively).

The module (driver IC) can be used with TTL compatible input signals. The input signals can also be driven with voltage levels that are lower than the VDD supply level. The VDD supply level does NOT affect the input threshold levels (VIH and VIL).



#### Figure 63. PWM threshold definitions

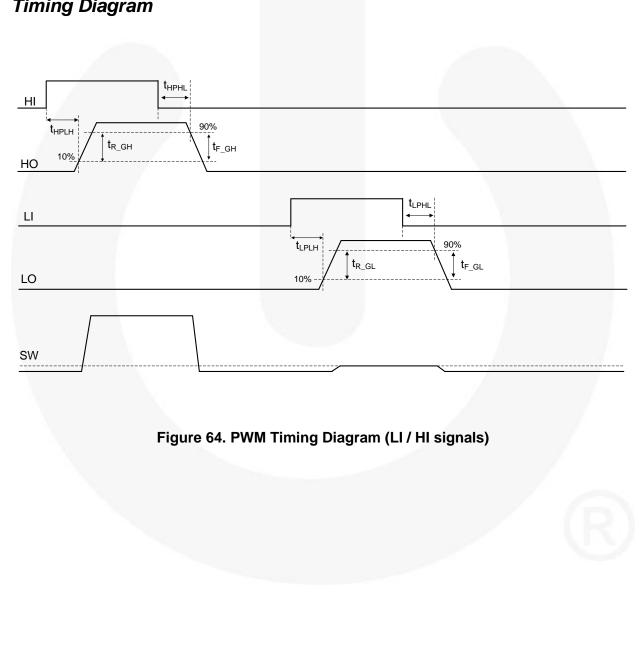
-  $V_{\text{IH}}$  = PWM trip level to flip state from LOW to HIGH.

-  $V_{IL}$  = PWM trip level to flip state from HIGH to LOW.

# Driver Output Stage

The driver IC output stage is designed to drive a pair of N-channel MOSFETs. The driver outputs (LO, HO) are non-inverting and will follow the PWM input commands (LI, HI respectively). The LO and HO outputs are capable of sinking and sourcing up to 0.65/0.35A peak current respectively.

The driver output stage is also capable of providing a rail (VDD) to rail (VSS) output voltage level when driving the Power MOSFETs. Depending on the end application, the output voltage level can be set to aide in optimizing MOSFET and driver IC power losses. The driver output voltage level can also be used to help adjust SW node edge rates.



# **Timing Diagram**

# **Application Information:**

The FDMF4061 is designed as a non-inverting power stage, where the Power MOSFET response (SW node) is designed to follow to HI/LI commands. The device is well-suited to be used in a wide variety of applications, such as: Half and Full-Bridge DC-DC converters. Active Clamp Forward converters, rectifier circuits, and motor drive power stages. However, various applications and topologies can place unique stresses on the module. few basic power-stage There are а needed requirements to ensure proper operation.

## Module Power Dissipation

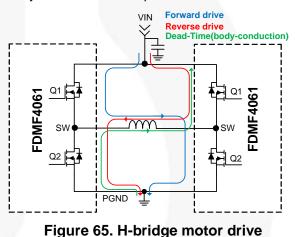
As previously mentioned, the FDMF4061 is a multi-chip module (MCM). The module consists of three die (HS MOSFET, LS MOSFET and driver IC). Each die dissipates heat in normal operation resulting from power loss. The power MOSFETs can generate power loss from conduction and switching losses while the driver IC dissipated loss from bias, boot diode conduction and from the driver output stage sinking and sourcing power gate currents and operating MOSFET frequency. The amount of heat dissipated by any die is largely dependent on the operating conditions. The close physical placement of the three die inside of the package translates into strong thermal coupling between die. Ideally, a thermal camera should be used to monitor the FDMF4061 during the engineering development phase. This can help ensure the module operates within the absolute maximum ratings specified in this datasheet.

# **Operating Modes**

The FDMF4061 can reliably operate while driving various load impedances. However, the relatively large number of applications can result in the module operating in various modes. Common applications such as switching power converters and motor drives can place the FDMF4061 into different operating modes. The various operating modes will change the response of the MOSFET voltage and current stresses and power losses as well as the gate driver dead time response. A few operating modes are listed below.

### **H-bridge Motor Drive**

In this operating mode, it allows bi-directional current flow through motor by enabling diagonal MOSFETs to make current flow in one or the other direction. Inductor current will not tolerate abrupt changes either when charged or discharged and alternate path is required to protect switches during dead-time. The path can be made either MOSFET body-diode conducting as soon as switches are disabled or enabling opposite high-side or low-side switch to carry the recirculation current while avoiding shootthrough. Utilizing MOSFET channel is often much more efficient way to handle the decaying current due to lower conduction power loss than body-diode forward drop loss.



#### FDMF4061 Power Dissipation

The maximum motor drive current can be obtained from estimating total power dissipation of motor driver. There are a number of factors which limit actual current level such as motor ratting, driver IC, PCB construction, ambient temperature and given application. All of power dissipation components must be considered to get reliable operation at the specific application. There is obvious power dissipations listed below in single H-bridge motor application.

Conduction loss – Generally biggest power loss which is dissipated due to the R<sub>DSON</sub> and its temperature coefficient must be considered in the calculation

 $\mathbf{P}_{\text{COND}} = (\mathbf{r}_{\text{DS(ON)}-\text{HS}_{\text{temp}}} + \mathbf{r}_{\text{DS(ON)}-\text{LS}_{\text{temp}}}) \cdot \mathbf{I}_{\text{OUT}}^{2}$ 

 Switching losses - Rising and falling time by parasitic inductance can be measured in the application, listed below assumed zero inductance.

#### Switching OFF loss

$$P_{SW(OFF)} = \left(\frac{V_{IN} \cdot I_{DS(OFF)} \cdot t_{OFF}}{2}\right) \cdot F_{SW}$$
  
where:  
$$t_{OFF} = (Q_{GS2} + Q_{GD})/i_{G(OFF)};$$
  
$$i_{G(OFF)} = V_{PLATEAU}/(R_{GH} + R_{DRV, OFF})$$

#### Switching ON loss

$$\begin{split} P_{SW(ON)} &= (\frac{V_{IN} \cdot I_{DS(ON)} \cdot t_{ON}}{2} + \frac{Qoss \cdot V_{IN}}{2}) \cdot F_{SW} \\ where: \\ t_{ON} &= (Q_{GS2} + Q_{GD})/i_{G(ON)}; \\ i_{G(ON)} &= V_{PLATEAU}/(R_{G} + R_{DRV\_ON}) \\ Qoss &= OutputCharge \end{split}$$

Gate drive loss

 $\mathbf{P}_{\mathrm{GATE}} = \mathbf{Q}_{\mathrm{G}} \cdot \mathbf{V}_{\mathrm{DRV}} \cdot \mathbf{F}_{\mathrm{SW}}$ 

 Quiescent current power loss – Current is still drawn from the VDD and HB pins for internal and level shifting circuitry without load (R<sub>G</sub>=Open). Power loss by quiescent current is

$$\mathbf{P}_{\text{Quiescent}} = \mathbf{V}_{\text{DD}} \cdot \mathbf{I}_{\text{DDQ}} + \mathbf{V}_{\text{HB}} \cdot \mathbf{I}_{\text{HBQ}}$$

Supply current power loss(R<sub>G</sub>=0Ω) is

 $P_{supply} \!=\! V_{DD} \cdot I_{DDO} + V_{HB} \cdot I_{HBO}$ 

 Total power loss in the FDMF4061 is equal to the power dissipation caused by gate driver and Power MOSFETs,

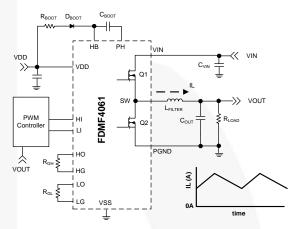
$$P_{\text{total}} = P_{\text{Cond}} + P_{\text{SW}} + P_{\text{Gate}} + P_{\text{supply}}$$

Once the designer estimates power dissipation in the gate driver and MOSFETs, junction temperature can be calculated using thermal resistance ( $\Theta_{JA}$ ) and ambient temperature as followings and also can calculate maximum allowable motor current:

$$T_j = T_A + (\Theta_{JA} \cdot P_{total})$$

# Continuous current flowing out of SW node.

Continuous current flowing out of the module SW node is typical of a heavily loaded switchedmode power stage that is operating in a synchronous buck converter topology. In this mode, the power stage is supplying current from VIN into an inductive load. **Figure 66** shows and example of a synchronous buck convert operating in CCM with positive inductor current.



#### Figure 66. Synchronous Buck Operating in CCM with positive inductor current

During this operating mode, the HS MOSFET (Q1) will undergo hard-switched inductive turn-on and turn-off events, while LS MOSFET (Q2) will undergo soft switching and body diode recovery. Hard-switching often results in large switching spikes on Q1 and Q2  $V_{DS}$  as well as PH to VSS and BOOT to VSS pins. Peak switching spikes are often positively correlated to load current.

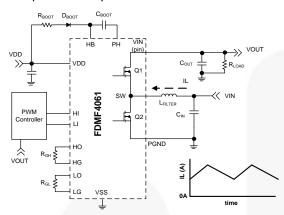
# Continuous current flowing into SW node.

Continuous current flowing into the module SW node is typical of a heavily loaded switched-mode power stage that is operating in a synchronous boost converter topology.

Continuous inductor current flowing in to the module SW node is typical operation of a

synchronous boost converter, as shown in **Figure 67**.

However, similar operation can arise when a switching converter (such as a synchronous buck) is pulling energy from the output filter capacitors and delivering the energy back to the input filter capacitors.



# Figure 67. Synchronous Boost Converter operating in CCM

From a module perspective, the main difference here versus the previous (buck) operating mode is that this situation will cause the LS FET (Q2) to act as the control MOSFET and hard switch while the HS FET (Q1) acts as a synchronous rectifier and undergoes soft switching with body diode recovery. This type of operation can drastically change power losses dissipated in Q1 and Q2 versus buck operating mode.

# dV<sub>DS</sub>/dt control using external gate resistors

The FDMF4061 also provides module pins for placing external gate resistors. The module provides pins for the HO and LO signals (driver output signals) and the HG and LG (Power MOSFET gate pins). Resistors can be placed in series with the MOSFET gate to control the SW node edge rates.

Independently controlling MOSFET (slower) turn-on and (faster) turn-off slew rates can also be accomplished by using the resistor and diode circuit shown in **Figure 68**.

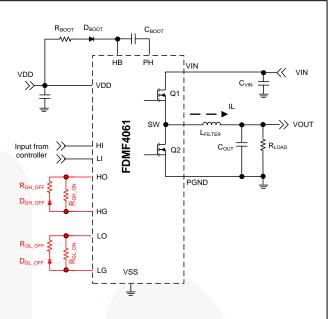
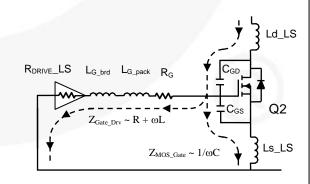


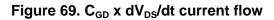
Figure 68. Gate drive resistor-diode circuit

# C<sub>GD</sub> x dV<sub>DS</sub>/dt turn-on

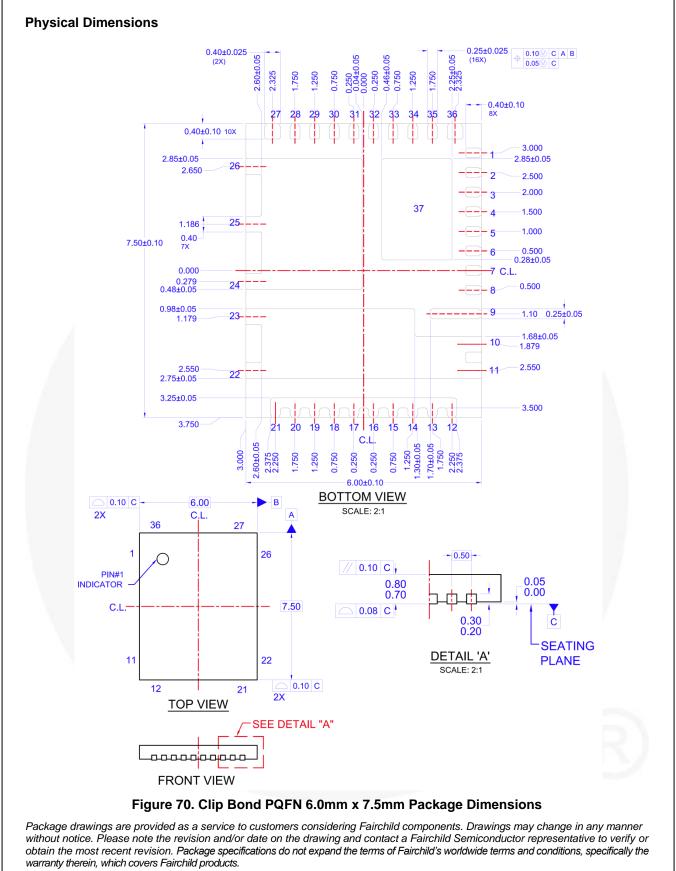
 $C_{GD} \times dV_{DS}/dt$  turn-on is a false (unwanted) turn-on event that often creates a brief and uncontrolled shoot through current between the HS (Q1) and LS (Q2) MOSFETs.

Typically, a  $C_{GD} \times dV_{DS}/dt$  "shoot-through" condition arises from capacitive feedback current flowing through  $C_{GD}$  into  $C_{GS}$  inducing a gate-bounce-induced channel turn-on of the MOSFET. Holding the gate below threshold can become challenging because the high-frequency capacitive displacement current from  $C_{GD}$  (due to  $dV_{DS}/dt$ ) couples back to circuit ground through the gate electrode.

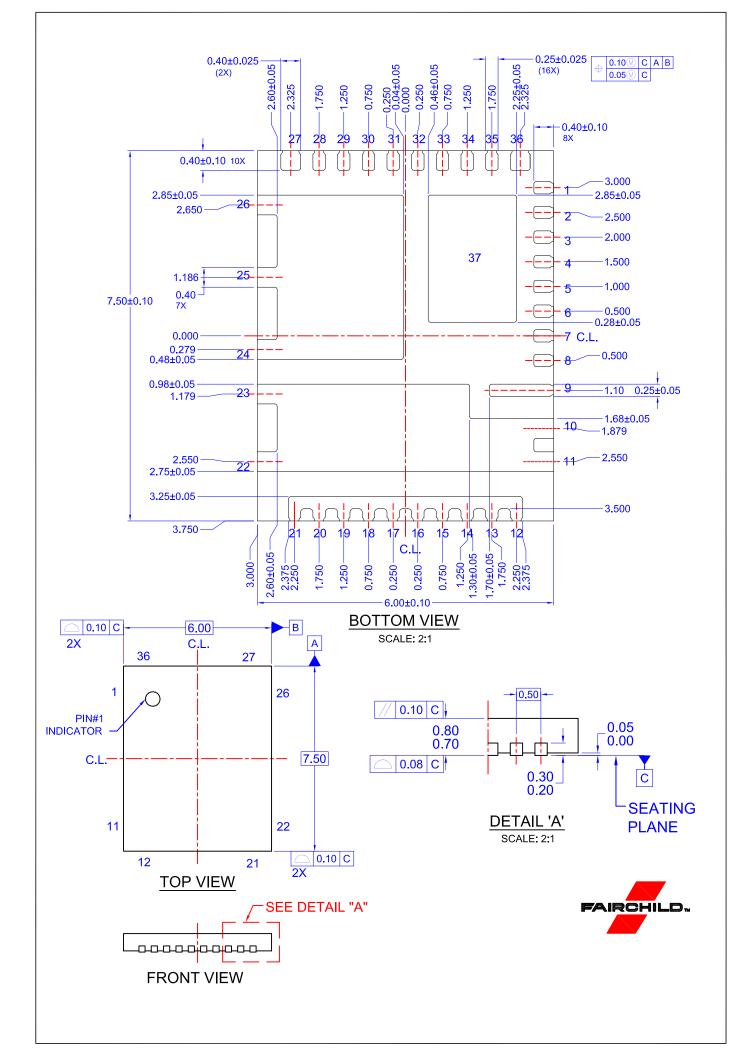


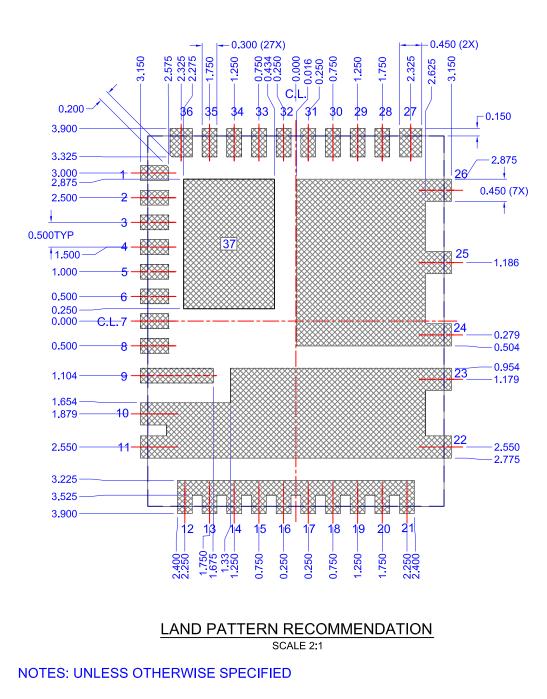


The gate-to-ground impedance is the parallel combination of the gate drive  $(Z_{G_DRV})$  and the MOSFET gate-to-source  $(Z_{MOS_Gate})$  paths. As  $dV_{DS}/dt$  increases, the more favorable path for displacement current is through the capacitive gate-source  $(C_{GS})$  path versus the highly inductive and resistive gate drive loop. So impedence through gate driver should be minimized. The severity of the shoot through current is difficult to predict.



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